



Analytical investigation of nanoparticle migration in a duct considering thermal radiation

Zhixiong Li^{1,2} · S. Saleem³ · Ahmad Shafee⁴ · Ali J. Chamkha^{5,6} · Sunwen Du⁷

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Abstract

Buongiorno model is applied to investigate nanofluid migration through a permeable duct in the presence of external forces. Influences of radiation and Joule heating on first law equation are added. Final formulas are solved via differential transform method. Roles of suction, thermophoretic, radiation and Brownian motion parameters, Schmidt number, Hartmann number, Eckert number were presented. Results show that temperature gradient improves with the enhancement of Reynolds number, suction and Radiation parameters. Nu augments with the augmentation of Hartmann and Eckert numbers, while reverse behavior is seen for skin friction coefficient. Also, it can be concluded that Nusselt number enhances with the increase in radiation parameter but it decreases with the increase in Brownian motion.

Keywords Differential transform method · Porous duct · Nanoparticle · Lorentz forces · Buongiorno model

List of symbols

B_0 Magnetic induction (Tesla)
 Pr Prandtl number
 Rd Radiation parameter
 Ha Hartmann number
 C_p Specific heat capacity (J/kgK)
 v, u Vertical and horizontal velocities (m/s)

q_r Thermal radiation (W)
 T Fluid temperature (K)

Greek symbols

σ_e Stefan–Boltzmann constant
 μ Dynamic viscosity (Pa s)
 ϕ Volume fraction of nanofluid
 α Thermal diffusivity ($m^2 s^{-1}$)
 η Similarity-independent variable
 β_R Mean absorption coefficient
 σ Electrical conductivity

✉ Zhixiong Li
zhixiongli@cumt.edu.cn

- ¹ School of Engineering, Ocean University of China, Qingdao 266110, China
- ² School of Mechanical, Materials, Mechatronic and Biomedical Engineering, University of Wollongong, Wollongong, NSW 2522, Australia
- ³ Department of Mathematics, College of Science, King Khalid University, Abha 61413, Saudi Arabia
- ⁴ Public Authority of Applied Education & Training, College of Technological Studies, Applied Science Department, Shuwaikh, Kuwait
- ⁵ Mechanical Engineering Department, Prince Sultan Endowment for Energy and Environment, Prince Mohammad Bin Fahd University, Al-Khobar 31952, Saudi Arabia
- ⁶ RAK Research and Innovation Center, American University of Ras Al Khaimah, Ras Al Khaimah, United Arab Emirates
- ⁷ College of Mining Technology, Taiyuan University of Technology, Yingze West St. 79, Taiyuan 030024, P. R. China

Subscripts

T Thermal quantity
 f Base fluid

Introduction

Nanoscience can suggest applicable working fluid to improve thermal behavior. Karimipour et al. [1] investigated the impact of kind of nanoparticles on nanofluid MHD flow in a microchannel. Maleki et al. [2] simulated non-Newtonian nanofluid flow over a permeable plate. Sheikholeslami et al. [3] presented an experimental study to analyze exergy loss during condensation process. Hosseini et al. [4] offered the new method for estimating thermal conductivity of nanofluids. They used interfacial

shell-dependent dimensionless model. Esfahani et al. [5] investigated oil-based nanofluid transportation. They compared numerical result with experimental data. Sheikholeslami and Rokni [6] published a report for application ferrofluid. Comprehensive review paper has been published by Sheikholeslami and Ganji [7] to show importance of nanotechnology. Haq et al. [8] investigated carbon nanotube pulsatile flow due to magnetic forces in an annulus. Sheikholeslami [9] utilized nanoparticle-enhanced PCM for discharging process. He simulated this unsteady problem with FEM. Arani et al. [10] studied the heat transfer of carbon nanotubes (SWCNT) nanofluid in a heat sink.

Sheikholeslami et al. [11] simulated second law analysis of nanofluid forced convection in a heat exchanger. Khodabandeh et al. [12] investigated nanofluid flow in a horizontal spiral coil. This geometry can be used for solar ponds. Tao and He [13] presented the NEPCM charging process in an energy storage system. Ahmed et al. [14] reported time-dependent flow along a heated plate. Sheikholeslami et al. [15] investigated discharging process of NEPCM in the presence of thermal radiation. Alrashed et al. [16] presented a regression for characteristics of carbon-based nanofluid. Jafaryar et al. [17] investigated turbulent heat transfer in a pipe equipped with twisted tape. Nasiri et al. [18] utilized SPH for nanofluid flow over a cylinder. Sheikholeslami [19] employed magnetic field to expedite the solidification process. Goodarzi et al. [20] investigated two-phase flow of nanofluid in a cavity with lid wall. Sheikholeslami et al. [21] investigated three-dimensional MHD flow of nanofluid in a cubic cavity. They used mesoscopic approach. Selecting effective working fluid becomes hot topics in recent years [22–75].

In this paper, radiation of nanofluid through a permeable duct is investigated using DTM. Impacts of suction, radiation, Brownian motion and thermophoretic parameters, Schmidt and Hartmann, Eckert numbers have been presented.

Governing equation

Steady two-phase flow of nanofluid in a semipermeable duct is considered. Figure 1 shows the geometry and boundary conditions. Constant vertical magnetic field effect has been applied. Effects of Joule heating and radiation on temperature distribution are employed. The lower surface is hot, and the upper one is cold. Governing formulas are [22]:

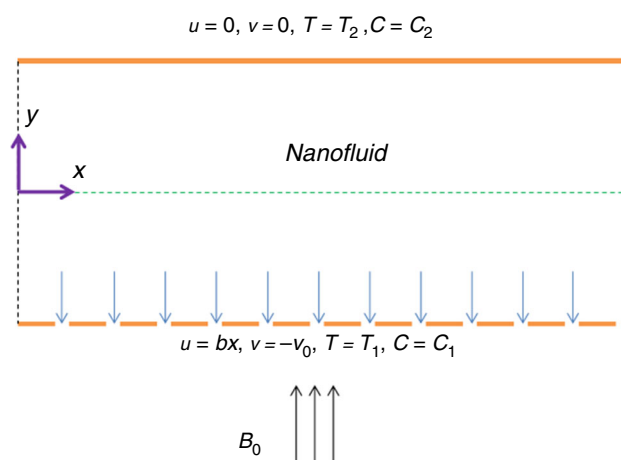


Fig. 1 Geometry of the problem

$$\frac{\partial v}{\partial y} + \frac{\partial u}{\partial x} = 0 \tag{1}$$

$$\rho_f \left(v \frac{\partial u}{\partial y} + u \frac{\partial u}{\partial x} \right) = \mu \left(\frac{\partial^2 u}{\partial y^2} \right) - \frac{\partial p}{\partial x} - \sigma B_0^2 u, \tag{2}$$

$$\rho_f \left(v \frac{\partial v}{\partial y} + \frac{\partial v}{\partial x} u \right) = - \frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 v}{\partial x^2} \right) \tag{3}$$

$$\begin{aligned} \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) (\rho C_p)_f &= k \left(\frac{\partial^2 T}{\partial y^2} \right) \\ &+ (\rho C_p)_p \left[D_B \left\{ \frac{dC}{dy} \cdot \frac{dT}{dy} \right\} \right. \\ &+ \left. (D_T/T_2) \left\{ \left(\frac{dT}{dy} \right)^2 \right\} \right] \\ &- \frac{\partial q_r}{\partial y} + \sigma B_0^2 u^2, \\ q_r &= - \frac{4\sigma_e}{3\beta_R} \frac{\partial T^4}{\partial y} \end{aligned} \tag{4}$$

$$\frac{\partial C}{\partial y} v + \frac{\partial C}{\partial x} u = \left(\frac{D_T}{T_2} \right) \left\{ \frac{d^2 C}{dy^2} \right\} + D_B \frac{\partial^2 C}{\partial y^2} \tag{5}$$

where according to [76], $T^4 \cong 4T_c^3 T - 3T_c^4$.

Boundary conditions are:

$$\begin{aligned} \text{at } y = -a \quad & C = C_1, \quad u = bx, \quad v = -v_0, \quad T = T_1, \\ \text{at } y = +a \quad & C = C_2, \quad v = 0, \quad u = 0, \quad T = T_2, \end{aligned} \tag{6}$$

The following definitions are used to convert equations to ODEs [22]:

$$\eta = \frac{y}{a}, \quad u = bx f'(\eta), \quad v = -abf(\eta), \quad \theta = \frac{T - T_1}{T_1 - T_2}, \tag{7}$$

$$\phi = \frac{C - C_1}{C_1 - C_2}$$

According to Eq. (7), final ODEs are:

$$f^{iv} + R(f'''f - f''f') - Ha^2 f'' = 0 \tag{8}$$

$$\left(1 + \frac{4}{3}Rd\right)\theta'' + Prf\theta' + Ha^2 Ec \frac{Pr}{R} f'^2 + Nb\theta'\phi' + Nt\theta'^2 = 0 \tag{9}$$

$$\phi'' + Sc(f\phi') + \frac{Nt}{Nb}\theta'' = 0 \tag{10}$$

where $R, Ha, Rd, Ec, Pr, Nt, Nb, Sc$ are:

$$R = \frac{a^2 b}{\nu}, \quad Ha = B_0 a \sqrt{\frac{\sigma}{\mu}}, \quad Rd = 4\sigma_c T_c^3 / (\beta_R k),$$

$$Ec = \frac{\rho_f (bx)^2}{(\rho C_p)_f \Delta T}, \quad Pr = (\rho C_p)_f \frac{a^2 b}{k},$$

$$Nt = \frac{\Delta T (\rho C_p)_p D_T}{(\rho C_p)_f \alpha}, \quad Nb = \Delta C \alpha^{-1} D_B (\rho C_p)_f^{-1} (\rho C_p)_p,$$

$$Sc = \frac{\nu}{D},$$

$$A_1 = \frac{\rho_{nf}}{\rho_f}, \quad A_2 = \frac{\mu_{nf}}{\mu_f}, \quad A_4 = \frac{k_{nf}}{k_f}, \quad A_3 = \frac{(\rho C_p)_{nf}}{(\rho C_p)_f}, \quad A_5 = \frac{\sigma_{nf}}{\sigma_f} \tag{11}$$

Moreover, at $\eta = 1, -1$ we have:

$$\theta(1) = 0, \quad \phi(1) = 0,$$

$$f(1) = 0, \quad f(-1) = \frac{\nu_0}{ab} = \lambda, \tag{12}$$

$$\phi(-1) = 1, \quad f'(-1) = 1,$$

$$f'(1) = 0, \quad \theta(-1) = 1$$

Nu and C_f over the bottom wall are

$$Nu = |\theta'(-1)|, \quad C_f = |f''(-1)| \tag{13}$$

Solution with differential transformation method

The basic idea of DTM exists in [23]. Applying the differential transforms for Eqs. (8–10) gives:

$$(k+3)(k+1)(4+k)(2+k)F[k+4] - Ha^2 f''(2+k)(k+1)F[2+k] - R \sum_{m=0}^k ((2+m)(1+m)F[m+2](k+1-m)F[k+1-m]) - R \sum_{m=0}^k ((3+m)(m+1)(2+m)F[3+m]F[-m+k]) = 0 \tag{14}$$

$$F[3] = a_4, \quad F[0] = a_1, \tag{15}$$

$$F[2] = a_3, \quad F[1] = a_2,$$

$$(1+k)\left(1 + \frac{4}{3}Rd\right)(2+k)\Theta[2+k] + Pr \sum_{m=0}^k (F[-m+k](1+m)\Theta[1+m]) + Ha^2 Ec \frac{Pr}{R} \sum_{m=0}^k ((1+m)F[-m+k+1](k-m+1)F[1+m]) + Nb \sum_{m=0}^k ((-m+k+1)\Theta1+m\Phi[-m+k+1]) + Nt \sum_{m=0}^k (\Theta[1+m](-m+k+1)\Theta[k-m+1](1+m)) = 0 \tag{16}$$

$$\Theta[0] = a_5, \quad \Theta[1] = a_6 \tag{17}$$

$$(2+k)(1+k)\Phi[1+k+1] + Sc \sum_{m=0}^k (F[-m+k]\Phi[m+1](1+m)) + (k+2)(1+k)\frac{Nt}{Nb}\Theta[k+2] = 0$$

$$+ Ha^2 Ec \frac{Pr}{R} \sum_{m=0}^k ((m+1)F[m+1](k-m+1)F[k-m+1]) + Nb \sum_{m=0}^k ((m+1)(k-m+1)\Phi[k-m+1]\Theta[m+1]) + Nt \sum_{m=0}^k ((-m+k+1)(m+1)\Theta[-m+k+1]\Theta[1+m]) = 0 \tag{18}$$

$$\Phi[0] = a_7, \quad \Phi[1] = a_8 \tag{19}$$

According to previous equations,

$$F[3] = a_4, \quad F[2] = a_3, \quad F[1] = a_2, \quad F[0] = a_1,$$

$$F[4] = \frac{1}{12}Ha^2 a_3 + \frac{1}{12}R a_2 a_3 - \frac{1}{4}R a_1 a_4, \tag{20}$$

$$F[5] = \frac{1}{20}Ha^2 a_4 + \frac{1}{30}R a_3^2 - \frac{1}{60}RHa^2 a_1 a_3 + \frac{1}{20}(R)^2 a_1^2 a_4, \dots$$

$$\begin{aligned} \Theta[0] &= a_5, \quad \Theta[1] = a_6, \\ \Theta[2] &= -1.5 \frac{1}{R(3 + 4Rd)} (Nt R a_6^2 + Pr a_1 a_6 R + Ha^2 Pr Ec a_2^2 \\ &\quad + Nb a_8 a_6 R), \dots \end{aligned} \tag{21}$$

$$\begin{aligned} \Phi[0] &= a_7, \quad \Phi[1] = a_8, \\ \Phi[2] &= \frac{0.5}{Nb R(3 + 4Rd)} (-3Sc a_1 a_8 Nb R - 4Sc a_1 a_8 Nb R Rd \\ &\quad + 3 Nt^2 a_6^2 R + 3 Nt Pr a_1 a_6 R + 3 Nt Nb a_6 a_8 R), \dots \end{aligned} \tag{22}$$

Finally, we have:

$$\begin{aligned} F(\eta) &= a_1 + a_2 \eta + a_3 \eta^2 + a_4 \eta^3 \\ &\quad + \left(\frac{1}{12} Ha^2 a_3 + \frac{1}{12} R a_2 a_3 - \frac{1}{4} R a_1 a_4 \right) \eta^4 + \dots \end{aligned} \tag{23}$$

$$\begin{aligned} \Theta(\eta) &= a_5 + a_6 \eta \\ &\quad + \left(\frac{-1.5}{R(3 + 4Rd)} (Nt R a_6^2 + Pr a_1 a_6 R + Ha^2 Pr Ec a_2^2 \\ &\quad + Nb a_8 a_6 R) \right) \eta^2 + \dots \end{aligned} \tag{24}$$

$$\begin{aligned} \Phi(\eta) &= a_7 + a_8 \eta \\ &\quad + \frac{0.5}{Nb R(3 + 4Rd)} (-3Sc a_1 a_8 Nb R \\ &\quad - 4Sc a_1 a_8 Nb R Rd + 3 Nt^2 a_6^2 R + 3 Nt Pr a_1 a_6 R \\ &\quad + 3 Nt Nb a_6 a_8 R) \eta^2 + \dots \end{aligned} \tag{25}$$

So, $a_1, a_2, a_3, a_4, a_5, a_6, a_7, a_8$ can be obtained. By inserting these values into Eqs. (23–25), the expression of $F(\eta), \Theta(\eta)$ and $\Phi(\eta)$ can be obtained which are the transformation of $f(\eta), \theta(\eta)$ and $\phi(\eta)$, respectively.

Results and discussion

Roles of external forces on two-phase flow of CuO–H₂O in a semipermeable duct with stretching wall are investigated. Influence of radiation and Joule heating on first law equation is employed. ODEs are obtained via similarity transformation and solved by differential transform method. Figure 2 illustrates the verifications of presented result with those of obtained in previous works [77,78].

Impact of Reynolds number on f, θ and ϕ is demonstrated in Fig. 3. Vertical velocity and θ profiles decrease with the increase in Re. Horizontal velocity near the

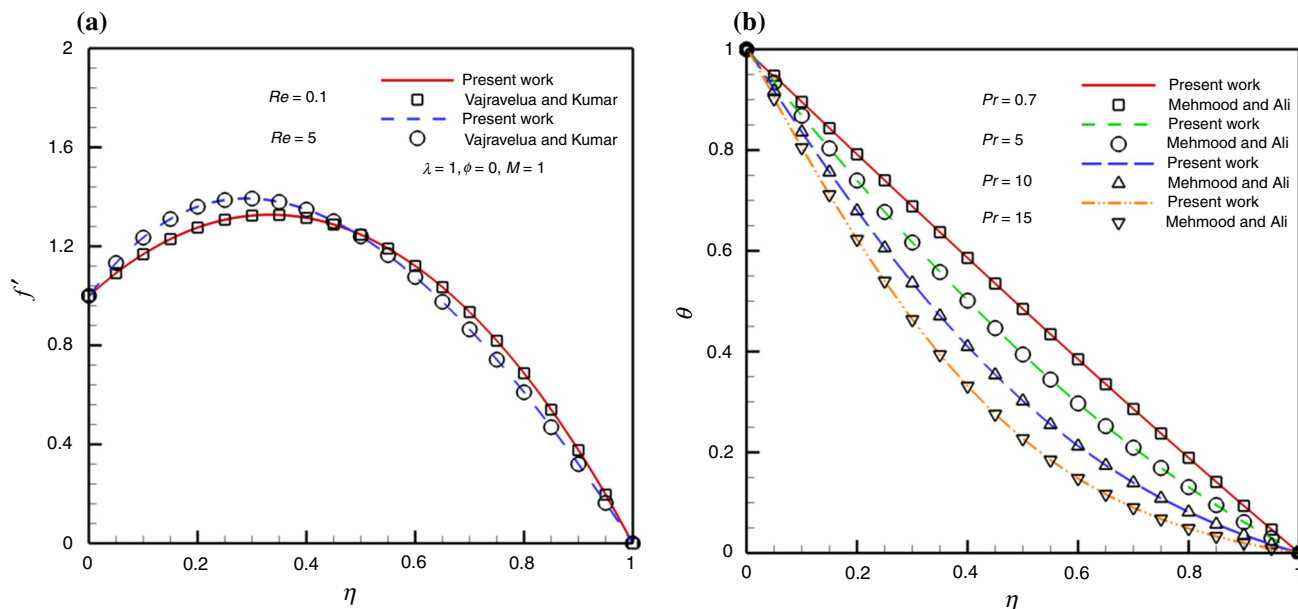


Fig. 2 Comparison of the velocity and temperature profiles between the present work and (a) [77]; b [78] for different values of Pr when $\lambda = 0.5, M = 1, R = 0.5$ and $Kr = 0.5$

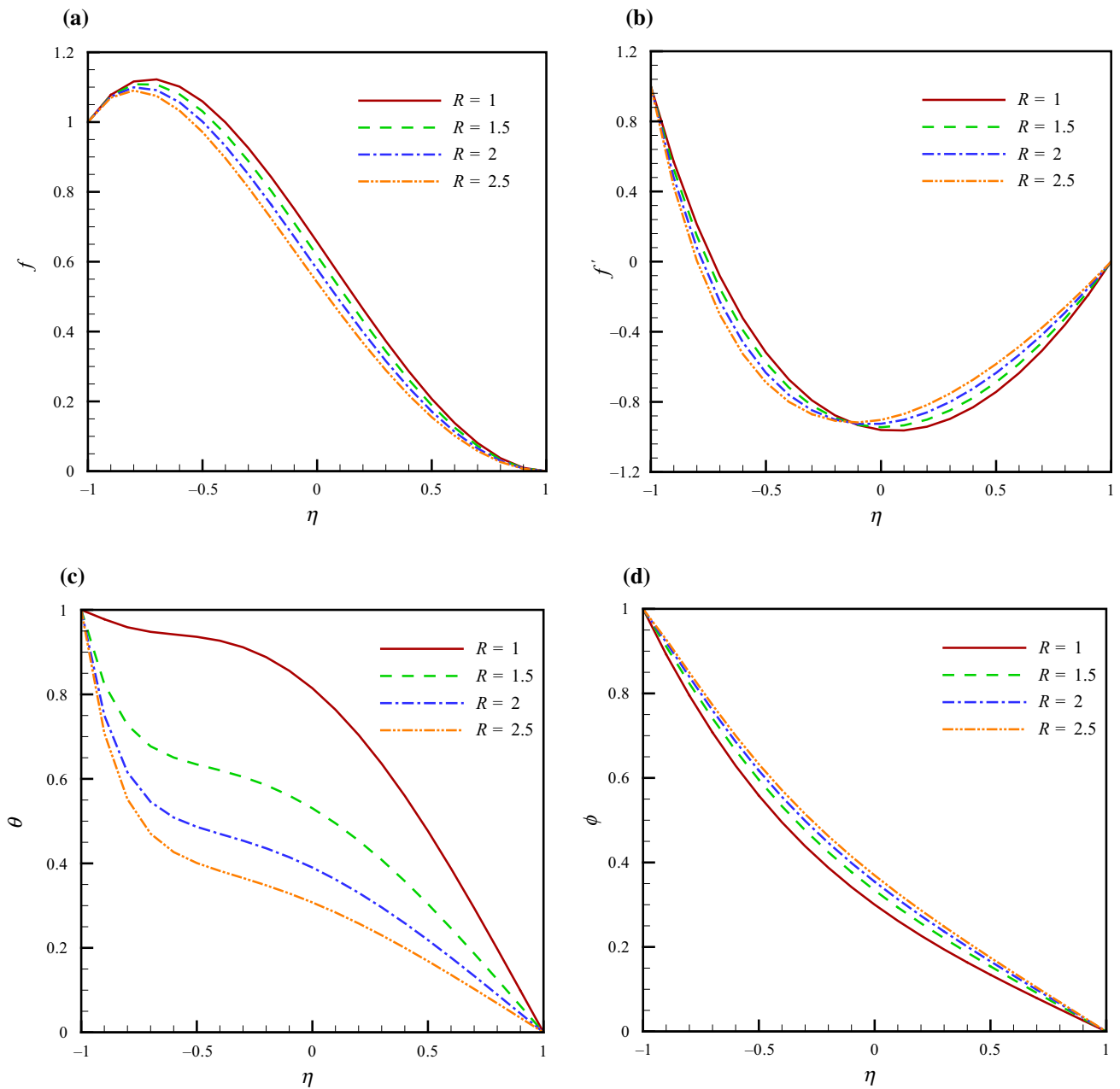


Fig. 3 Effect of Reynolds number on velocity, temperature, concentration profiles when $Ha = 1, \lambda = 1, Rd = 0.5, Ec = 0.5, Sc = 1, Nt = 0.001, Nb = 0.01, Pr = 10$

bottom wall decreases with the increase in Re , but reverse observation is seen next to upper wall. Also, ϕ increases with the augmentation of Re . Figure 4 illustrates the impact of Hartmann number on various profiles.

Temperature profile increases with the augmentation of Hartmann number. Also velocity detracts with the augmentation of Ha . Concentration profile improves with the augmentation of Hartmann number. Figure 5 illustrates the

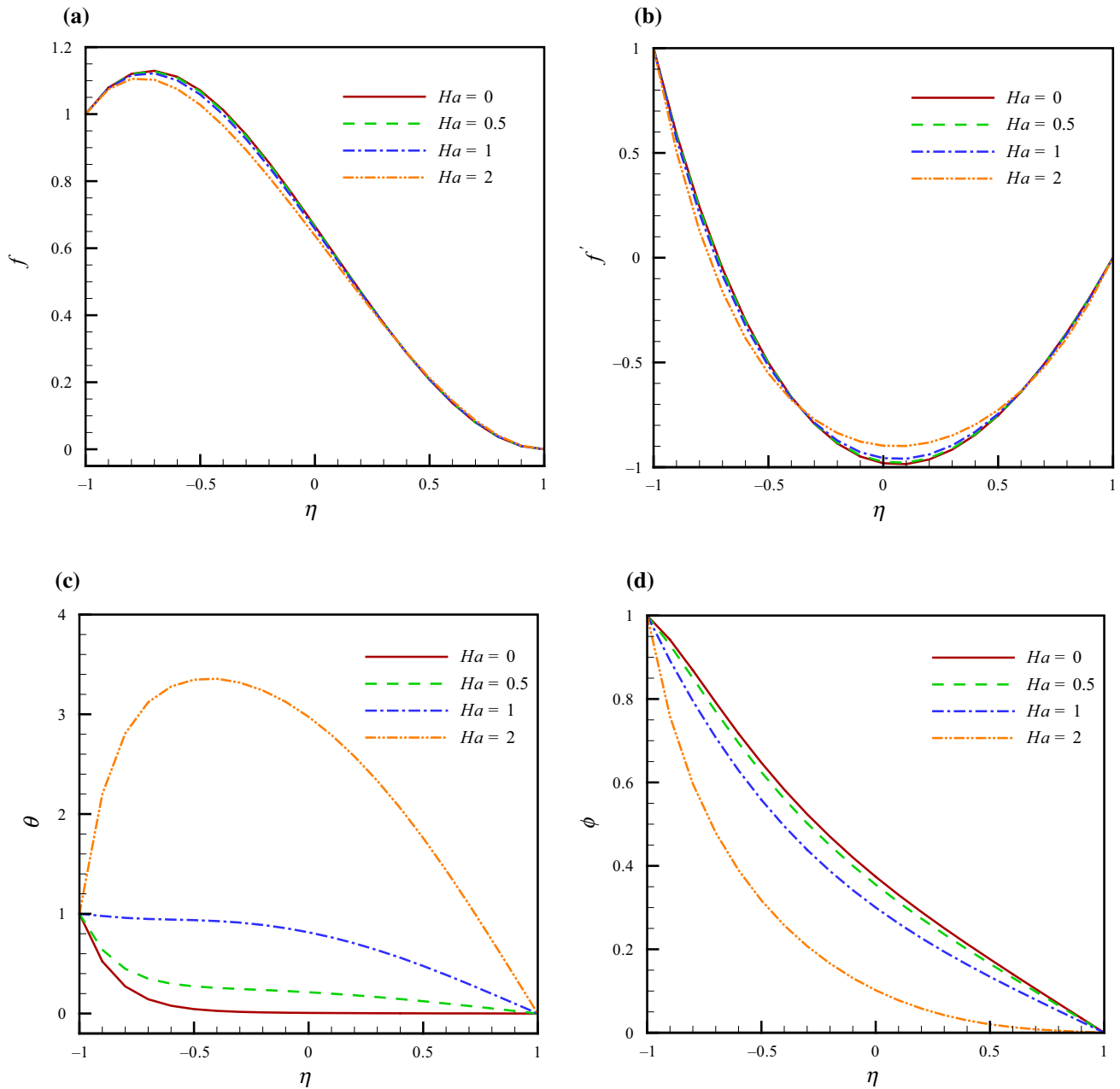


Fig. 4 Effect of Hartman number on velocity, temperature, concentration profiles when $R = 1, \lambda = 1, Rd = 0.5, Ec = 0.5, Sc = 1, Nt = 0.001, Nb = 0.01, Pr = 10$

roles of suction parameter on various profiles. Temperature and vertical velocity augment with the increase in suction parameter. Horizontal velocity detracts with the

augmentation of suction parameter. Also the minimum point of velocity shifts to lower wall. Also concentration has inverse relationship with suction parameter.

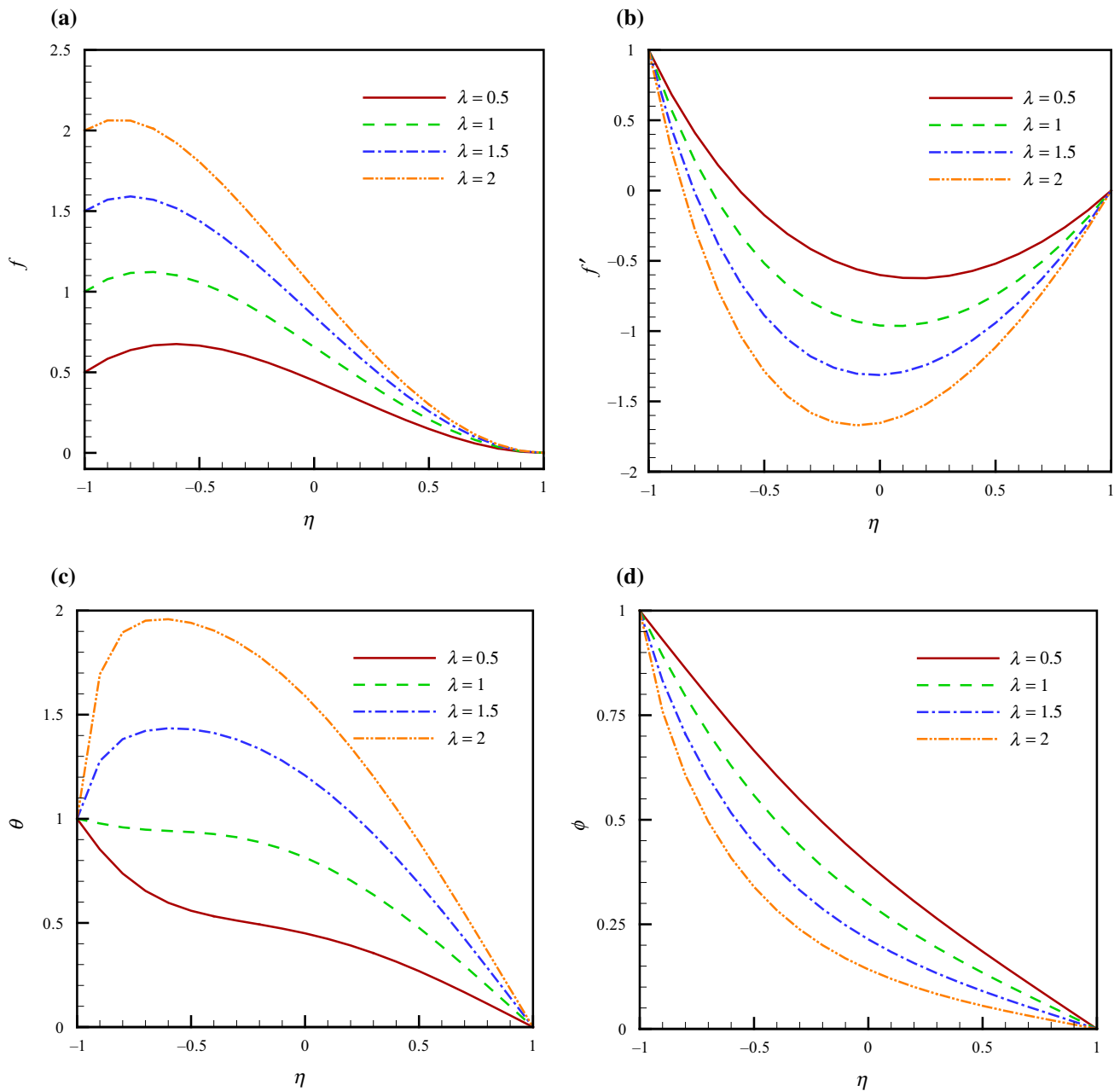


Fig. 5 Effect of suction parameter on velocity, temperature, concentration profiles when $R = 1, Ha = 1, Rd = 0.5, Ec = 0.5, Sc = 1, Nr = 0.001, Nb = 0.01, Pr = 10$

Figure 6 illustrates the roles of radiation on θ profile. θ decreases with the augmentation of Rd . Figure 7 illustrates the impact of Eckert number on θ and ϕ profiles. As Ec

augments, the viscous dissipation augments and in turn θ augments with the increase in this parameter. Concentration detracts with the increase in Eckert number. Figure 8

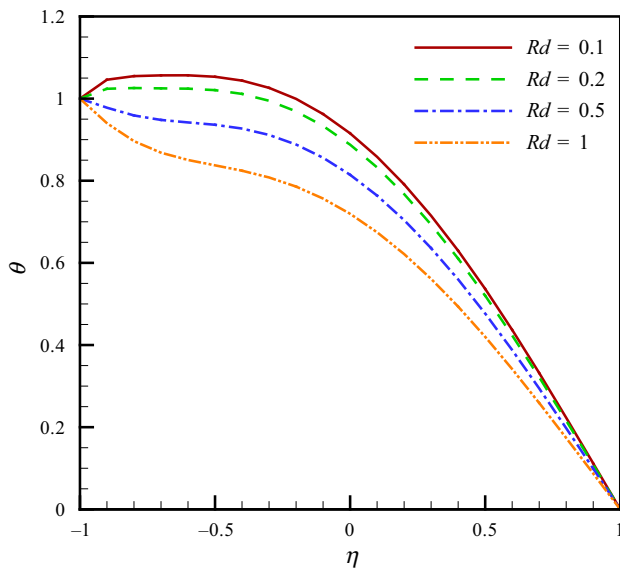


Fig. 6 Effect of radiation parameter on temperature profile when $R = 1, Ha = 1, \lambda = 1, Ec = 0.5, Sc = 1, Nt = 0.001, Nb = 0.01, Pr = 10$

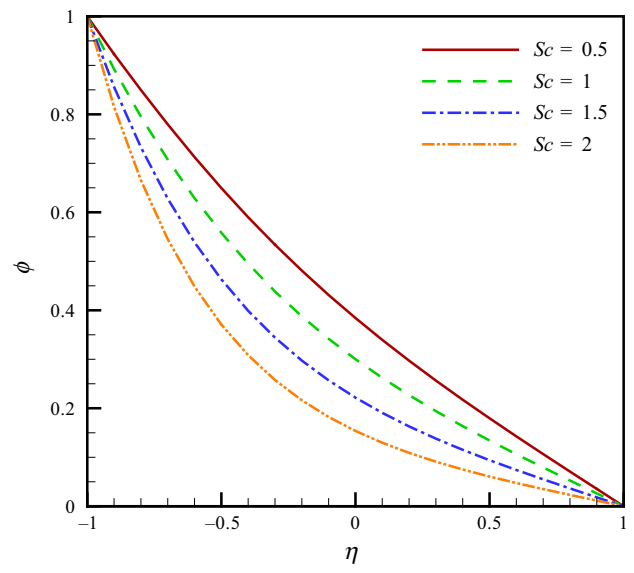


Fig. 8 Effect of Schmidt number on concentration profile when $R = 1, Ha = 1, \lambda = 1, Rd = 0.5, Ec = 0.5, Nt = 0.001, Nb = 0.01, Pr = 10$

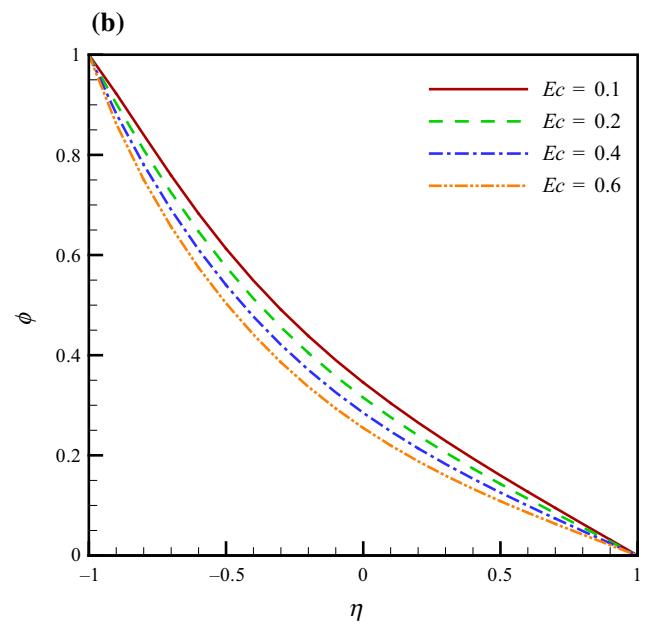
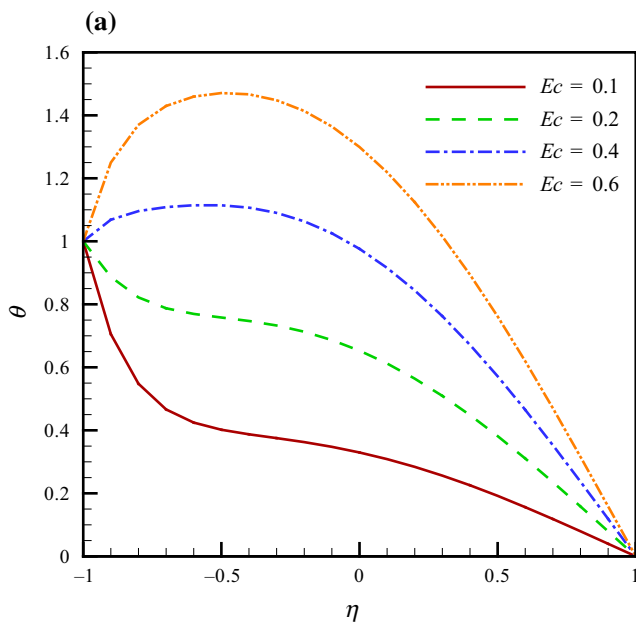


Fig. 7 Effect of Eckert number on temperature and concentration profiles when $R = 1, Ha = 1, \lambda = 1, Rd = 0.5, Sc = 1, Nt = 0.001, Nb = 0.01, Pr = 10$

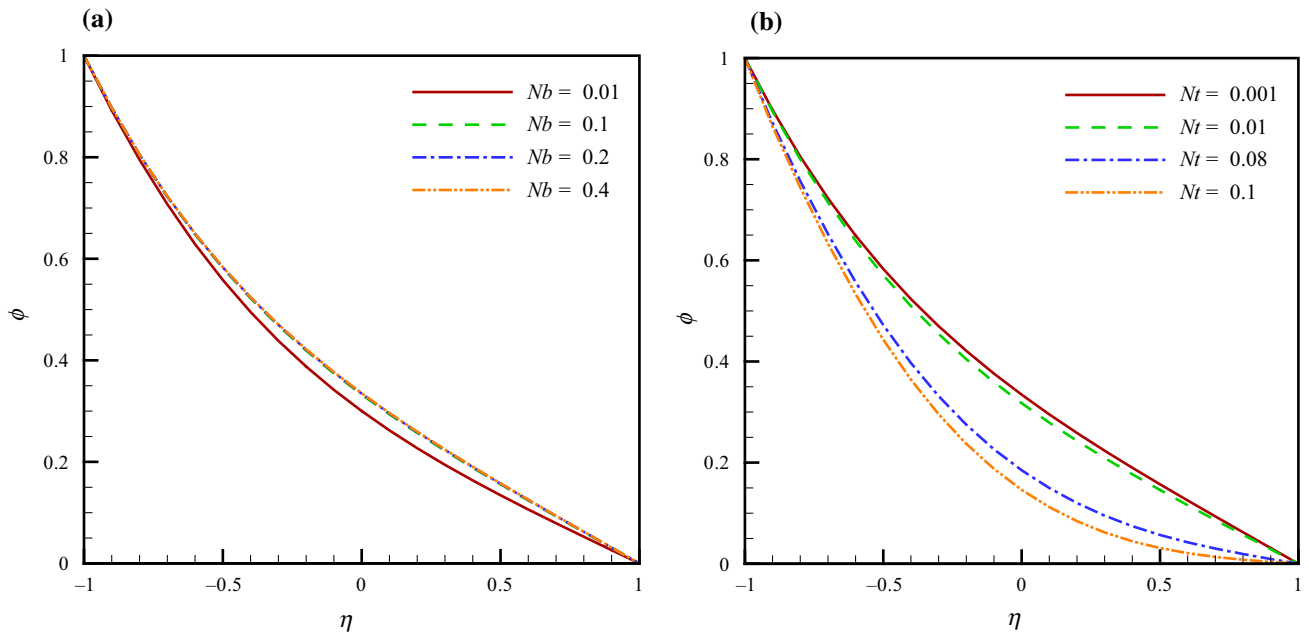


Fig. 9 Effects of Brownian motion parameter and thermophoretic parameter on concentration profile when $R = 1, Ha = 1, \lambda = 1, Rd = 0.5, Ec = 0.5, Sc = 1, Pr = 10$ **a** $Nt = 0.001$ **b** $Nb = 0.01$

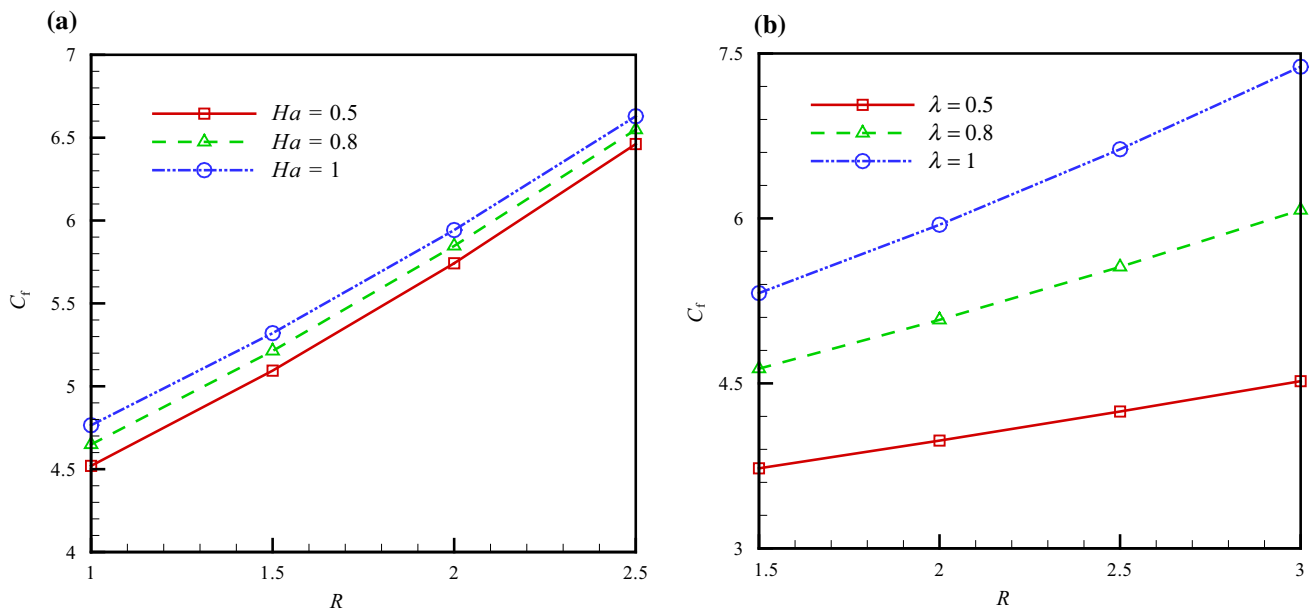


Fig. 10 Effects of suction parameter, Reynolds number, Hartman number on skin friction coefficient **a** $\lambda = 1$ **b** $Ha = 1$

illustrates the impact of Sc on ϕ profile. Increasing Schmidt number causes ϕ to decrease. Figure 9 demonstrates the impacts of Nb and Nt on ϕ profile. ϕ augments with the

increase in Nb , while it decreases with the augmentation of Nt . Figure 10 exhibits the influences of suction parameter, Re , and Hartman number on C_f . C_f augments with the

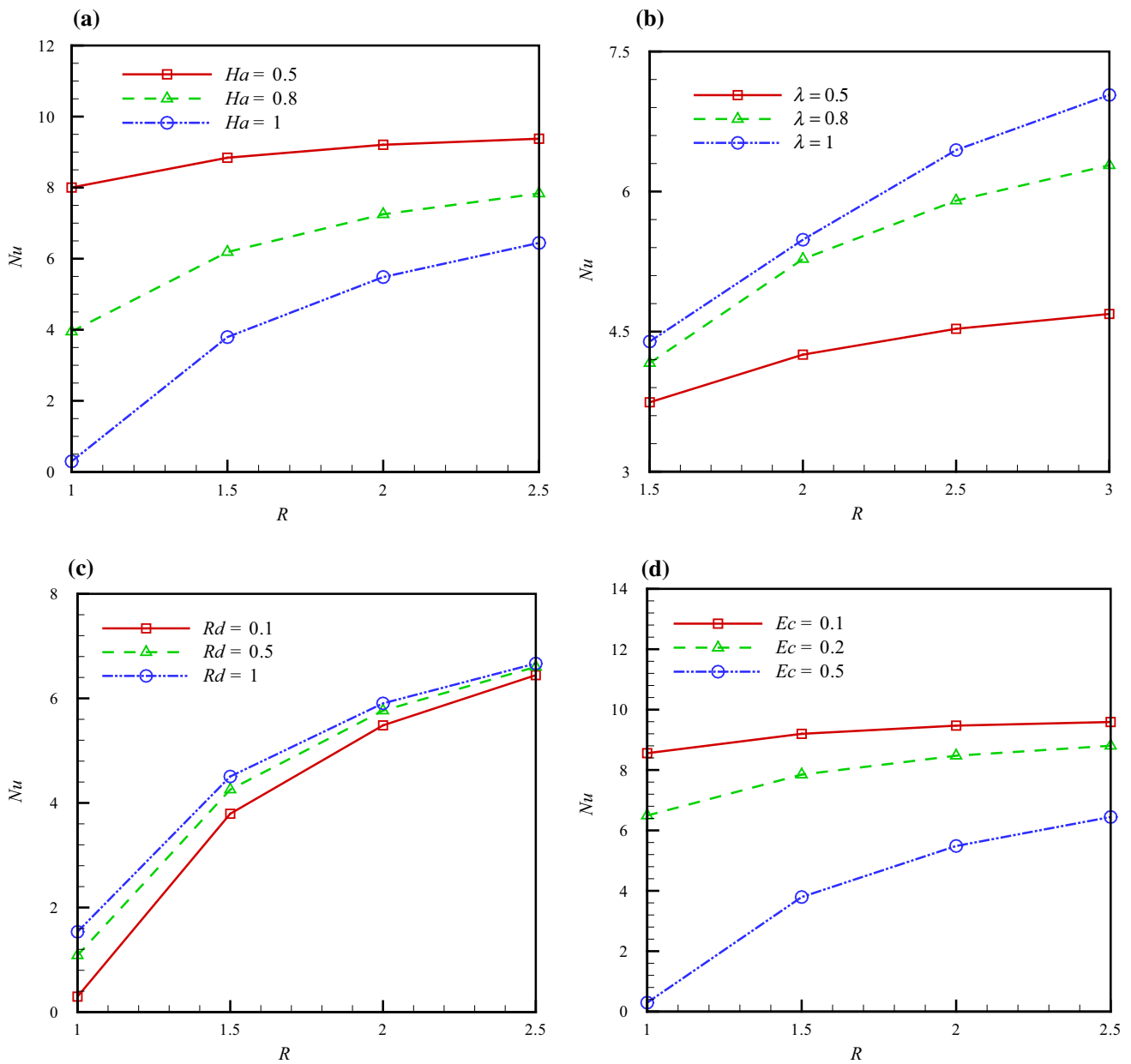


Fig. 11 Effects of Hartmann number, Eckert number, suction parameter, radiation parameter, Reynolds number on Nusselt number when **a** $\lambda = 1, Rd = 0.5, Ec = 0.5$ **b** $Ha = 1, Rd = 0.5, Ec = 0.5$ **c**

$Ha = 1, \lambda = 1, Ec = 0.5$ **d** $Ha = 1, \lambda = 1, Rd = 0.5, Sc = 1, Nt = 0.001, Nb = 0.01, Pr = 10$

increase in suction parameter, Re , and Hartman number. Figure 11 depicts the impact of Hartmann number, Eckert number, suction parameter, Rd, Re on Nu . Nu augments with the increase in Rd , suction parameter and Re . θ'

decreases with the augmentation of Lorentz forces and Eckert number. Tables 1 and 2 depict the influence of Nb and Nt on Nu . Nu detracts with the augmentation of these parameters.

Table 1 Effect of Brownian motion parameter on Nusselt number when $Ha = 1$, $\lambda = 1$, $Rd = 0.5$, $Ec = 0.5$, $Sc = 1$, $Nr = 0.001$, $Pr = 10$

Nu	Nb		
	0.001	0.04	0.08
R			
1	0.30306	0.275026	0.243478
1.5	3.801208	3.76956	3.733913
2	5.49183	5.458464	5.420864
2.5	6.452456	6.4181	6.379375

Table 2 Effect of thermophoretic parameter on Nusselt number when $Ha = 1$, $\lambda = 1$, $Rd = 0.5$, $Ec = 0.5$, $Sc = 1$, $Nb = 0.2$, $Pr = 10$

Nu	Nt		
	0.001	0.05	0.07
R			
1	0.160723	0.117474	0.099823
1.5	3.640233	3.60063	3.584447
2	5.321965	5.28489	5.269732
2.5	6.277456	6.242033	6.227547

Conclusions

Differential transform method is utilized to analyze two-phase nanofluid magnetohydrodynamic flow through a semipermeable duct. Roles of radiation, Brownian motion, suction and thermophoretic parameters, Schmidt number, Hartmann number, Eckert number have been examined. As Hartman number and Eckert number augment, Nu decreases while reverse trend is reported for C_f . Besides it can be reported that Nu improves with increase in Re, Rd and suction parameter but it decreases with the increase in Nb and Nt parameters.

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